



## Unification of Pressure Systems in Deep Drawing Utilizing Lateral Fluid Pressure

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## Unification of Pressure Systems in Deep Drawing Utilizing Lateral Fluid Pressure

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The original equipment of the drawing utilizing lateral fluid pressure and the operation were simplified by unifying two pressure systems: punch pressure system and lateral pressure system. In the improved equipment, punch is forced down by punch rod which receives fluid pressure equal to lateral fluid pressure  $p_s$ . So, punch force  $F_p$  varies in proportion to  $p_s$  during the drawing process. The drawing characteristics in the improved equipment were given experimentally as  $p_s$ - $S$  curves, where  $S$  is punch stroke. The curves were analyzed based on results in the original equipment, and it was confirmed that the improved equipment is regulated according to its theory. The improvement of equipment may make this drawing more practical.

### 1. Introduction

Authors<sup>1~5)</sup> have already reported results of a series of studies on the deep drawing utilizing lateral fluid pressure. The drawing equipment has two pressure systems: punch pressure system, lateral fluid pressure system. The relation between those pressures during the drawing process was clarified experimentally for aluminum blank and was confirmed theoretically. In this deep drawing, remarkable reduction of punch load due to applying lateral fluid pressure enabled one to draw a blank with very high drawing ratio. However, the equipment and the operation were complicated because of having two pressure systems. This study was carried out to simplify the equipment and the operation by unifying the pressure systems.

### 2. Experimental Procedure

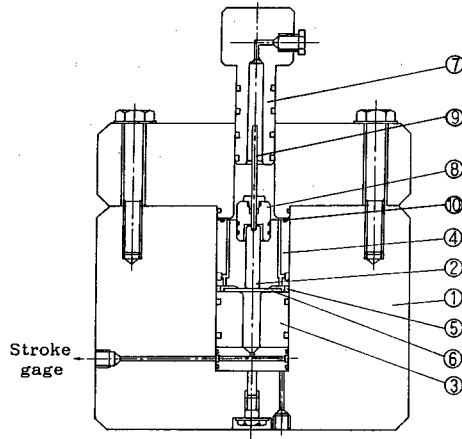
#### 2.1 Experimental equipment

Figures 1 and 2 show diagram of the improved drawing equipment and the magnified diagram of its improved part, respectively. In this equipment, well-balanced forces are applied simultaneously to the punch and side face of a blank by only pressurizing an unified fluid pressure system.

As shown in these figures, the intermediate cylinder of this equipment differs from that of original one<sup>1)</sup> in construction. In the original equipment, the intermediate cylinder separates the punch pressure system from the lateral pressure system, and the punch is operated directly by fluid pressure in the punch pressure system. In the improved equipment, the intermediate cylinder is pierced by the punch rod, and fluid pressure is sealed by the O-ring with backup ring that is fixed by the bushing on the

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- ① Container    ② Punch    ③ Die    ④ Hold-down cylinder
- ⑤ Stop ling   ⑥ Blank   ⑦ Plunger   ⑧ Intermediate cylinder
- ⑨ Punch rod   ⑩ Elastic ring

Fig. 1 Diagram of improved drawing equipment.

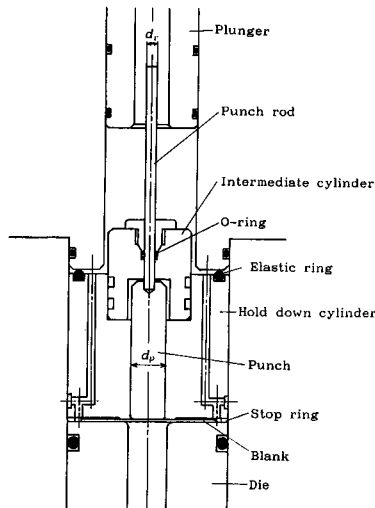


Fig. 2 Magnified diagram of improved part of drawing equipment.

intermediate cylinder. Therefore, the punch is operated indirectly by pressurizing the punch rod and the pressure is as same as lateral fluid pressure. Then, punch force  $F$  is given by  $F = p_s \cdot \pi d_r^2 / 4$  ( $d_r$ : punch rod diameter), and varies in proportion to lateral fluid pressure  $p_s$  during the drawing process.

Though the punch dose not receive directly fluid pressure in this equipment, equivalent punch pressure  $p_p'$  is defined by the following equation as what corresponds to punch pressure  $p_p$  in the original equipment.

$$p_p' = p_s (d_r^2 / d_p^2). \tag{1}$$

2.2 Experimental condition

For the specimen, the soft aluminum sheet A1050P-O of 0.8 mm in thickness was used and its mechanical properties are shown in Table 1. The diameter of blank  $D_0$  was 60 mm.

Table 2 shows main dimensions of tools. Punch diameter  $d_p$  was 15 mm, then drawing ratio  $D_0/d_p$  becomes 4. Diameter of punch rods  $d_r$  was determined based on the results of experiment with the original equipment<sup>1)</sup> in the range in which punch force will not cause fracture of a blank. Tools except the punch rod and intermediate cylinder were as same as those of the original equipment.

Let  $k$  be ratio of equivalent punch pressure  $p_p'$  to lateral fluid pressure  $p_s$ . Then,

$$k = p_p'/p_s = d_r^2/d_p^2 \tag{2}$$

Hereafter, the ratio  $k$  will be referred to as pressure ratio. As seen from Eq. (2), the thicker punch rod  $d_r$  gives the larger pressure ratio  $k$ . Pressure ratios for three punch rods R-1, R-2 and R-3 were 0.071, 0.090 and 0.111, respectively.

Table 1 Mechanical properties of specimen.

Material	A1050P-O
Tensile strength $\sigma_t$ /MPa	80
Elongation $e_f$ %	50
Strain hardening exponent $n$	0.28

Table 2 Main dimensions of tools

Punch	Diameter $d_p$ /mm		Punch profile radius $\rho_p$ /mm
	15.0		2.0
Punch rod	Diameter $d_r$ /mm		
	R-1	4.0	
	R-2	4.5	
	R-3	5.0	
Die	Die throat diameter $d_d$ /mm		Die profile radius $\rho_d$ /mm
	16.9		2.5
Hold-down cylinder	Protrusion		
	Diameter $d_h$ /mm	Height $h$ /mm	Taper angle $\theta/^\circ$
	26	0.1	7
Stop ring	Thickness $T$ /mm		
	0.85		

### 3. Results and Consideration

#### 3.1 Curve of $p_p$ - $S$ obtained in original equipment

Figure 3 shows curves of punch pressure  $p_p$  – punch stroke  $S$  representing drawing characteristics in the original equipment. These  $p_p$ - $S$  curves don't differ noticeably from those for the specimen used in previous paper<sup>1)</sup>. From this figure, it is seen that the minimum lateral fluid pressure  $p_s$  required to draw a blank without fracture is 110 MPa and the maximum punch pressure  $p_{pmax}$  for  $p_s = 110$  MPa is 13.6 MPa. Then,  $p_p/p_s$  becomes 0.124.

Therefore, pressure ratio  $k$  ( $= p_p'/p_s$ ) in the improved equipment must be under 0.124, and it is seen that diameter of punch rod  $d_r$  must be under 5.27 from Eq. (2). However, too thin punch rod is in danger of buckling. From the above, diameter of punch rod  $d_r$  was determined to be 4.0, 4.5 and 5.0 mm as shown in Table 2.

#### 3.2 Curve of $p_p$ - $S$ obtained in improved equipment

Figure 4 shows curves of lateral fluid pressure  $p_s$  – punch stroke  $S$  representing

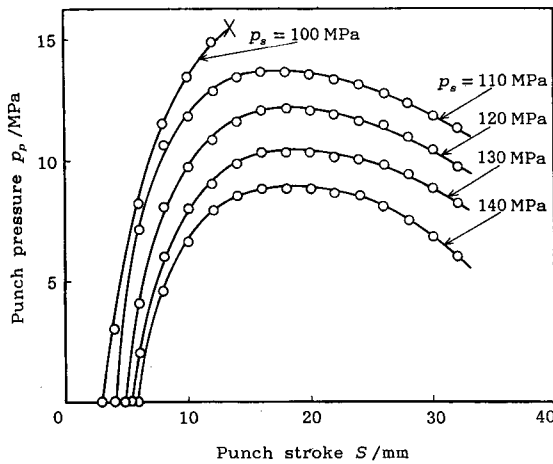


Fig. 3  $p_p$ - $S$  curves for different lateral fluid pressure  $p_s$  obtained in original equipment.

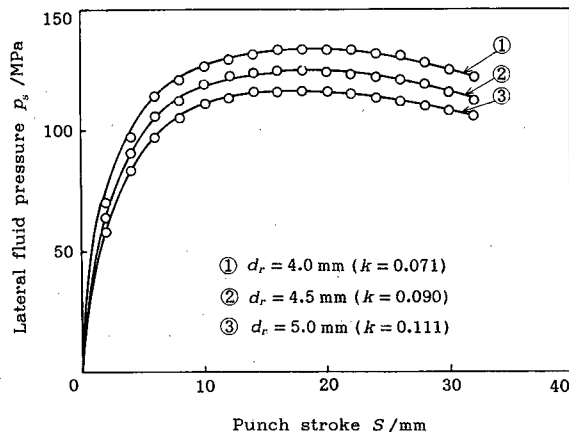


Fig. 4  $p_s$ - $S$  curves for different diameter of punch rod  $d_r$  obtained in improved equipment.

drawing characteristics in the improved equipment. These curves obtained for three different-diam punch rods are distinguished as curves ①, ② and ③. As shown in Fig. 4, the higher lateral fluid pressure is required for the thinner punch rod during the drawing process. In every curve, lateral fluid pressure  $p_s$  required to draw a blank increases rapidly at the beginning of drawing. Then, it increases slowly to a maximum and decreases gradually with increasing punch stroke  $S$ .

### 3.3 Curve of $p_p'-S$

Figure 5 shows curves of equivalent punch pressure  $p_p'$  – punch stroke  $S$ , which is obtained by transformation of  $p_s-S$  curves (Fig. 4) using Eq. (1). As shown in Fig. 5, when thinner punch rod is used, equivalent punch pressure  $p_p'$  becomes lower. On the other hand,  $p_p'-S$  curves may be estimate from  $p_p-S$  curves obtained in the original equipment as follows.

The diagram of  $p_p-S$  shown in Fig. 3 can be transformed into  $p_p-p_s$  diagram for different punch strokes  $S$ . Fig. 6 shows the  $p_p-p_s$  diagram for only  $S = 10, 20$  and  $30$  mm. As shown in this figure, the point at which  $p_p/p_s$  is equal to a pressure ratio  $k (= p_p'/p_s$ ; see Fig. 5) can be marked on the  $p_p-p_s$  curve for each punch stroke, and the value of

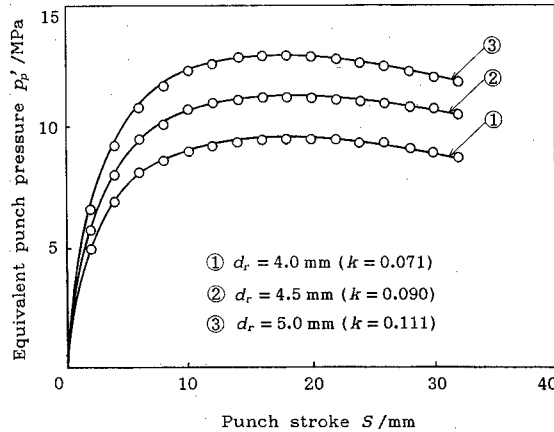


Fig. 5  $p_p'-S$  curves obtained in improved equipment.

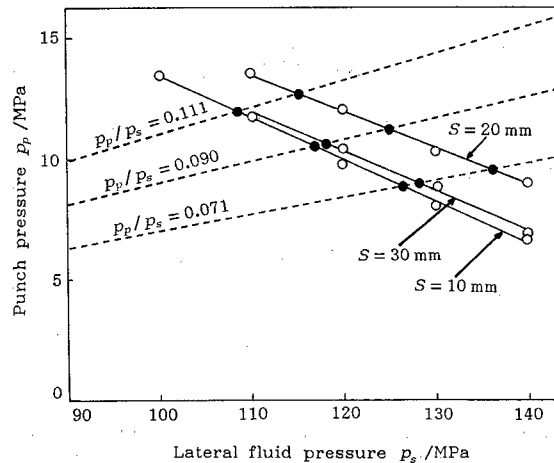


Fig. 6  $p_p-p_s$  diagram transformed from  $p_p-S$  diagram.

punch pressure  $p_p$  at the point can be read. The values read from many  $p_p$ - $p_s$  curves for different punch strokes were plotted on the  $p_p$ - $S$  diagram, and the points obtained were connected. The broken lines in Fig. 7 show the curves obtained by such a manner and they correspond to  $p_p'$ - $S$  curves estimated from  $p_p$ - $S$  curves. The estimated  $p_p'$ - $S$  curves (broken lines in Fig. 7) and the  $p_p'$ - $S$  curves obtained in improved equipment (Fig. 5) are compared in Fig. 8. As a result, it is confirmed that the both (solid lines and broken lines) coincide well.

### 3.4 Drawing force $F$ and its components $F_s$ and $F_p$

In the improved equipment, lateral fluid pressure  $p_s$  and punch force  $F_p$  vary proportionally during the drawing process. However, degrees of their contributions to drawing deformation are not seen easily, and evaluation of magnitude of total force required to draw a blank is difficult, because the force is applied dually to different parts of a blank.

Authors have already defined the drawing force in the deep drawing utilizing lateral

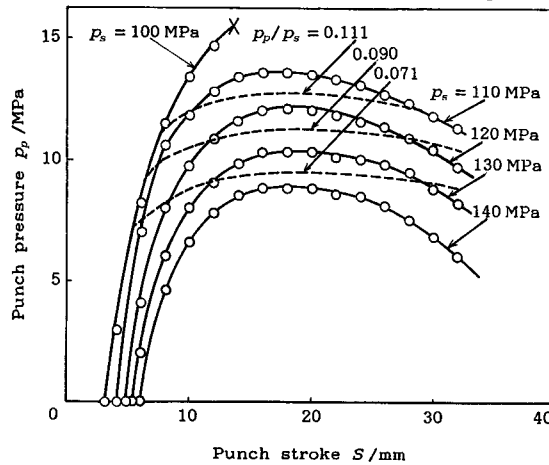


Fig. 7  $p_p'$ - $S$  curves estimated from  $p_p$ - $S$  curves obtained in original equipment.

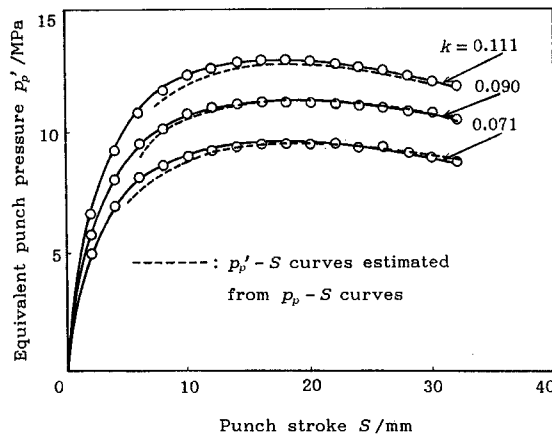


Fig. 8 Comparison of  $p_p'$ - $S$  curves obtained in improved equipment with those estimated from  $p_p$ - $S$  curves.

fluid pressure as the derivative of drawing work with respect to punch stroke<sup>3~5</sup>). By this definition, forces applied dually can be unified, and the drawing force  $F$  corresponds to the punch force in conventional drawing. Drawing force  $F$  in the improved equipment is given as a sum of punch force  $F_p$  and another component  $F_s$  caused by lateral fluid pressure  $p_s$  as shown by the following:

$$F = (\pi d_r^2/4)p_s + \pi d_t t p_s = F_p + F_s. \quad (3)$$

Where,  $d_t$  is the average of punch diameter  $d_p$  and die throat diameter  $d_d$ , and  $t$  is thickness of blank. Here, it is assumed that  $t$  is constant during the drawing process.

Figure 9 shows the variation of drawing force  $F$  and its component  $F_s$  caused by lateral fluid pressure during the drawing process in the improved equipment, which is obtained from Fig. 4 by using Eq. (3). As shown in Fig. 9,  $F$ - $S$  curves for different diameter of punch rod almost coincide, which suggests that the force required to draw a blank dose not depend on pressure ratio  $k$ . For smaller diameter of punch rod  $d_r$ , degree of punch force  $F_p$  ( $= F - F_s$ ) in drawing force  $F$  is smaller as a matter of course.

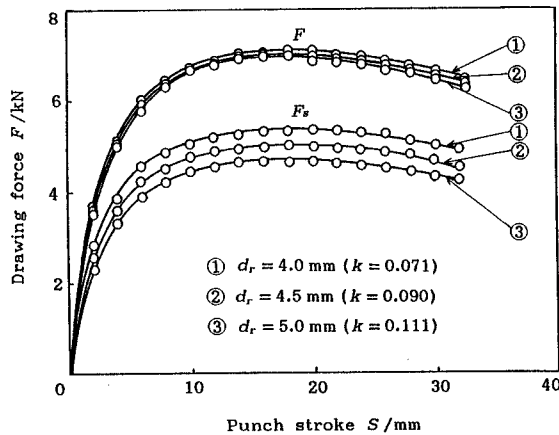


Fig. 9  $F$ - $S$  curves and  $F_s$ - $S$  curves obtained in improved equipment.

#### 4. Conclusion

Two pressure systems of the original equipment of the drawing utilizing lateral fluid pressure were unified to simplify the equipment and the operation. In the improved equipment, the punch is forced down by the punch rod which receives fluid pressure equal to lateral fluid pressure  $p_s$ . So, punch force  $F_p$  varies in proportion with  $p_s$  during the drawing process. The drawing characteristics in the improved equipment were given experimentally as  $p_s$ - $S$  curves. The curves were analyzed based on results in the original equipment, and it was confirmed that the improved equipment is regulated according to its theory. The improvement of equipment may make this drawing more practical.

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